- 1. Put a permanent magnet near a coil of wire carrying some variable current. Suppose the ferromagnetic material of the magnet is so hard that its magnetization **M** stays constant despite the variable **H** field of the coil.
  - (a) Argue that changing the current in the coil or moving the coil relative to the magnet takes reversible net work,

$$W_{\text{electric}} + W_{\text{mechanic}} = \Delta U(I, \text{coil's position}).$$
 (1)

for some well-defined magnetic energy U — there is no irreversibly lost work due to hysteresis. Also, show that the magnetic energy U for this system is is

$$U = \frac{\mu_0}{2} \iiint_{\text{whole space}} \mathbf{H}^2 d^3 \mathbf{x} + \text{const.}$$
 (2)

Now consider a system of several permanent magnets, each having constant magnetization **M** despite the **H** fields from the other magnets. But there are no coils or other macroscopic electric currents.

- (b) Argue that the magnetic forces and torques on the magnets follow from the potential energy U(geometry) which has exactly the same form as in eq. (2).
- (c) Show that without macroscopic currents

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$$\iiint\limits_{\text{whole space}} \mathbf{H} \cdot \mathbf{B} \, d^3 \mathbf{x} = 0, \tag{3}$$

then use this formula to rewrite the magnetic energy (2) as

$$U = -\frac{\mu_0}{2} \sum_{i \neq j}^{\text{magnets}} \iiint_{\text{magnet} \# i} \mathbf{M} \cdot \mathbf{H}[\text{magnet} \# j] d^3 \mathbf{x} + \text{const.}$$
 (4)

(d) To check this formula, consider a system of two small magnets separated by a much larger distance. Approximating each magnet as a pure dipole of magnetic moment

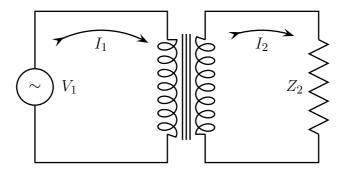
 $\mathbf{m}_1$  or  $\mathbf{m}_2$ , show that for this system

$$U + \text{const} = -\mathbf{B}_1 \cdot \mathbf{m}_2 = -\mathbf{B}_2 \cdot \mathbf{m}_1 \tag{5}$$

where  $\mathbf{B}_1$  is the magnetic field of the first magnet at the location of the second magnet and likewise for the  $\mathbf{B}_2$ . Then use eq. (5) to argue that the forces and the torques on the magnets stemming from the magnetic energy (4) = (5) agree with the usual formulae for the forces and the torques on magnetic dipoles,

$$\mathbf{F} = \nabla(\mathbf{m} \cdot \mathbf{B}), \quad \vec{\tau} = \mathbf{m} \times \mathbf{B}.$$
 (6)

2. A transformer is made of 2 coils on a common ferromagnetic core. The coils have respective self-inductances  $L_1$  and  $L_2$  and mutual inductance  $M_{12} = M_{21} = k\sqrt{L_1L_2}$ . The primary coil is plugged into an AC power source of voltage  $V_1$  and frequency  $\omega$ , while the secondary coil is connected to a load of impedance  $Z_2$ :



For simplicity, consider an ideal transformer: perfectly linear ferromagnetic core with no hysteresis, no eddy currents in the core, no ohmic losses in the wiring of the coils, and perfect magnetic coupling of the two coils, k = 1.

(a) Write down linear equations for the complex amplitudes of the currents in the two coils and the voltages on them. Then solve the equations and show that

$$\frac{V_2}{V_1} = n, \quad \frac{I_2}{I_1} = \frac{1}{n} \times \frac{j\omega L_2}{j\omega L_2 + Z_2}$$
 (7)

for stepping ratio

$$n = \sqrt{\frac{L_2}{L_1}} \tag{8}$$

In particular, show that even for an ideal transformer, the simple ratios

$$\frac{V_2}{V_1} = n, \quad \frac{I_2}{I_1} = \frac{1}{n} \tag{9}$$

obtain only for  $|Z_2| \ll \omega L_2$ .

(b) Now consider a somewhat less ideal transformer with a coupling coefficient k just a little bit smaller than 1, so that  $1 - k^2 \ll 1$ . Again, calculate the transformer ratios  $V_2/V_1$  and  $I_2/I_1$  and show that they approximate the simple ratios (9) for the load impedance  $Z_2$  in the range

$$\omega L_2 \gg |Z_2| \gg (1 - k^2) \times \omega L_2, \tag{10}$$

but outside of this range we need more complicated formulae.

(c) Finally, for a transformer made of two coils of respectively  $N_1$  and  $N_2$  turns wound around a toroidal ferromagnetic core, check that  $n \approx N_2/N_1$ . Also, explain what causes k < 1 and argue that in the limit of very high permeability  $\mu$  of the ferromagnetic core  $k \to 1$ .